

SEPARATOR FOR FUEL CELL AND SOLID POLYMER TYPE FUEL CELL

USIND SAID SEPARATOR

Background of the Invention

5 1. Field of the Invention

The present invention relates to a separator for fuel cell. More particularly, the present invention relates to a separator for fuel cell which has sufficient strength and gas non-permeability even when made in a thin sheet.

10 2. Description of the Prior Art

Fuel cell separators are generally a flat sheet having a plurality of parallel grooves on one or both sides and have a role of (1) transmitting the electricity generated in the gas-diffusing electrode of fuel cell, to outside and also (2) draining the water formed in the grooves during the process of electricity generation, and securing the grooves as passages for reactant gas flowing into the fuel cell.

As fuel cells have become lighter and thinner in recent years, it has become necessary to produce the separators therefore in a thinner sheet. However, the fuel cell

separators produced in a thinner sheet have had low strength and high gas permeability.

In order to solve the above problems, there were proposed a fuel cell separator which is a molding made of a carbon powder-phenolic resin mixture with an internal mold release agent, metal sheet between compressive conductive sheets, bonding them under pressure, and, simultaneously therewith, forming gas passages by punching (see U.S.P. No. 5,527,363).

In the fuel cell separator which is a molding made of a carbon powder-phenolic resin mixture with an internal mold release agent included, containing a metal mesh or a metal piece in the center, there are the same problems as seen in conventional separators; that is, the metal mesh or the metal piece tends to peel in the molding owing to the external force (e.g. impact or clamping) applied at the time of assembling of fuel cell, resulting in higher conductivity and gas permeability.

In the fuel cell separator obtained by inserting a metal sheet between compressive conductive sheets, bonding

them under pressure, and, simultaneously therewith, forming gas passages by punching, the conductive sheet and the metal sheet are bonded simply by pressure and the adhesion strength between them is insufficient; therefore, they may be separated from each other when used in hot water. Moreover, since the adhesion between the conductive sheet and the metal sheet is insufficient, the contact resistance between them is high, and the resulting fuel cell separator has high resistance and shows severe change with time particularly in hot water.

Summary of the Invention

The present invention intends to alleviate the above-mentioned problems of the prior art and provide a separator for fuel cell which has sufficient strength and gas impermeability even when made in a thin sheet.

According to the present invention, there is provided a separator for fuel cell, comprising

a conductive core part composed of a metal material or a metal composite material,

a conductive adhesive layer covering the conductive

core part, and

a conductive skin part formed on the conductive adhesive layer,

wherein the conductive core part and the conductive skin part

5 are bonded via the conductive adhesive layer, and the conductive skin part selectively contains a mold release agent.

Brief Description of the Drawings

Fig. 1 is a sectional view showing an example of
10 the structure of the fuel cell separator of the present invention.

Fig. 2 is a conceptual view showing an example of the process for production of the present fuel cell separator.

Fig. 3 is a conceptual view showing an example of
15 the process for production of the present fuel cell separator.

Fig. 4 is a conceptual view showing an example of the process for production of the present fuel cell separator.

In Fig. 1, numeral 1 refers to a conductive core part; numeral 2 refers to a conductive adhesive layer; numeral 3 refers to a conductive skin part; and numeral 4
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refers to a passage for reactant gas.

Detailed Description of the Invention

The present invention is hereinafter described in
5 detail.

The separator for fuel cell according to the pre-
sent invention comprises, as shown in, for example, Fig. 1, a
conductive core part 1 composed of a metal material or a
metal composite material, a conductive adhesive layer 2 cov-
10 ering the conductive core part 1, and a conductive skin part
3 formed on the conductive adhesive layer 2. In Fig. 1, 4 is
each passage for reactant gas flowing into fuel cell.

The shape of the present fuel cell separator is
not restricted to one shown in Fig. 1 and may be, for example,
15 such that has passages 4 for reactant gas at the upside as
well.

The conductive core part 1 is composed of a metal
material represented by titanium, aluminum, stainless steel
or the like, or a metal composite material obtained by coat-
20 ing a noble metal, a carbon material or the like on the above

metal material.

As the shape of the conductive core part 1, there can be mentioned, for example, a sheet-like shape having a thickness of about 5 μm to 3 mm, as shown in Fig. 1; a shape
5 corresponding to fuel cell separator; and a shape partly corresponding to fuel cell separator.

The conductive core part 1 may be subjected to a surface treatment by mechanical grinding such as sandblasting, discharge treatment, lapping, polishing or the like, in order
10 to allow the conductive core part 1 to have higher adhesivity to the conductive skin part 3 described later.

In Fig. 1, the conductive adhesive layer 2 covering the conductive core part 1 is composed of a conductive adhesive, so that the conductive skin part 3 containing a
15 mold release agent is bonded to the conductive core part 1. As the conductive adhesive, there can be mentioned, for example, a carbon-containing conductive adhesive comprising a carbon powder acting as a conductive filler and a resin acting as a binder.

20 The carbon powder acting as a conductive filler

in the conductive adhesive has no particular restriction as to the kind as long as it can be used for imparting conductivity. There can be mentioned, for example, natural graphite (e.g. scaly graphite or lumpy graphite), artificial graphite, expanded graphite, acetylene black, carbon black and Ketjen Black. They can be used singly or in combination of two or more kinds.

The carbon powder in the conductive adhesive preferably has an average particle diameter of 20 μ m or less, and the conductive adhesive layer 2 preferably has a thickness of 0.1 to 200 μ m. When the average particle diameter of the carbon powder is more than 20 μ m, uniform thickness could not be achieved, as a result, uniform conductivity may not be expected and peeling of the conductive skin part may be involved. When the thickness of the conductive adhesive layer is more than 200 μ m, deterioration of the conductivity may occur and no sufficient adhesive strength can be obtained.

The resin acting as a binder in the conductive adhesive has no particular restriction as to the kind as long as it can be used for conductivity improvement and also for

the strong bonding between the skin part and the core part.
There can be mentioned, for example, at least one kind selected from thermosetting resins, thermoplastic resins and rubbers. The resin may be a liquid or an emulsion.

5 As the thermosetting resin, there can be mentioned, for example, phenolic resin, polycarbodiimide resin, furfuryl alcohol resin, epoxy resin, cellulose, urea resin, melamine resin, unsaturated polyester resin, silicone resin, diallyl phthalate resin, bismaleimide triazine resin, polyami-
10 nobismaleimide resin and aromatic polyimide resin. They can be used singly or in admixture of two or more kinds.

 As the thermoplastic resin, there can be mentioned, for example, polyethylene, polystyrene, polypropylene, polymethyl methacrylate, polyethylene terephthalate, polybutylene terephthalate, polyethersulfone, polycarbonate, polyoxamethylene, polyamide, polyimide, polyamideimide, polyvinyl alcohol, polyvinyl chloride, polyphenylsulfone, polyether ether ketone, polysulfone, polyether ketone, polyarylate, polyetherimide, polymethylpentene, fluororesin, polyoxybenzoyl ester resin, liquid crystal polyester resin, aromatic

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polyester, polyacetal, polyallylsulfone, polybenzimidazole, polyethernitrile, polythioethersulfone and polyphenylene ether. They can be used singly or in admixture of two or more kinds.

5 As the rubber, there can be mentioned, for example, fluororubber, silicone rubber, butyl rubber, chloroprene rubber, nitrile rubber, nitrile-chloroprene rubber, chlorinated butyl rubber, epichlorohydrin rubber, epichlorohydrin-ethylene oxide rubber, epichlorohydrin-ethylene oxide-acrylic
10 glycidyl ether terpolymer, urethane rubber, acrylic rubber, ethylene-propylene rubber, styrene rubber, butadiene rubber and natural rubber. They can be used singly or in admixture of two or more kinds.

 The conductive adhesive may contain, as necessary,
15 additives such as dispersing agent, thickening agent, stabilizer, antifoaming agent and the like.

 In the conductive adhesive, the proportions of the carbon powder and the resin can be, for example, 100 parts by weight (the carbon powder) and 10 to 150 parts by
20 weight (the resin). When the proportion of the resin is

smaller than 10 parts by weight, no sufficient adhesive layer is obtained. When the proportion of the resin is larger than 150 parts by weight, no sufficient conductivity is obtained.

The carbon powder and the resin can be simply mixed, whereby the conductive adhesive can be obtained. The application of the conductive adhesive to the conductive core part 1 to form a conductive adhesive layer 2 for covering the conductive core part 1 can be conducted by a known method such as casting, dip coating, spraying, brush coating, screen printing or the like. The thus-applied conductive adhesive may be introduced, in that state, into a step of bonding with the conductive skin part 3 described later, or may be dried and cured in, for example, a drier. The drying temperature employed in this drying step can be, for example, 30 to 200°C.

In the present invention, the conductive skin part containing a mold release agent 3 has a function of allowing the separator to have a lower contact resistance with a material with which the separator comes in contact, such as film electrode, carbon paper or the like. As the material constituting the conductive skin part 3, there can be men-

tioned a carbon-containing composite material containing a carbon powder as a conductive filler and a resin as a binder.

In the material constituting the conductive skin part 3, the carbon powder as a conductive filler has no particular restriction as to the kind as long as it can impart conductivity. As the carbon powder, there can be mentioned, as in the above-mentioned conductive adhesive, for example, natural graphite (e.g. scaly graphite or lumpy graphite), artificial graphite, expanded graphite, acetylene black, carbon black and Ketjen Black. They can be used singly or in combination of two or more kinds.

The carbon powder in the conductive skin part preferably has an average particle diameter of 30-100 μ m for high conductivity.

In the material constituting the conductive skin part 3, the resin as a binder has no particular restriction as to the kind as long as it can improve the conductivity and strength of skin part. As the resin, there can be mentioned, as in the conductive adhesive, for example, at least one kind selected from thermosetting resins, thermoplastic resins and

rubbers. The resin may be a liquid or an emulsion.

As the thermosetting resin, there can be mentioned, for example, phenolic resin, polycarbodiimide resin, furfuryl alcohol resin, epoxy resin, cellulose, urea resin, melamine resin, unsaturated polyester resin, silicone resin, diallyl phthalate resin, bismaleimidetriazine resin, polyaminobismaleimide resin and aromatic polyimide resin. They can be used singly or in admixture of two or more kinds.

As the thermoplastic resin, there can be mentioned, for example, polyethylene, polystyrene, polypropylene, polymethyl methacrylate, polyethylene terephthalate, polybutylene terephthalate, polyethersulfone, polycarbonate, polyoxamethylene, polyamide, polyimide, polyamideimide, polyvinyl alcohol, polyvinyl chloride, polyphenylsulfone, polyetherether ketone, polysulfone, polyether ketone, polyarylate, polyetherimide, polymethylpentene, fluororesin, polyoxybenzoyl ester resin, liquid crystal polyester resin, aromatic polyester, polyacetal, polyallylsulfone, polybenzimidazole, polyethernitrile, polythioethersulfone and polyphenylene ether. They can be used singly or in admixture of two or

more kinds.

As the rubber, there can be mentioned, for example, fluororubber, silicone rubber, butyl rubber, chloroprene rubber, nitrile rubber, nitrile-chloroprene rubber, chlorinated butyl rubber, epichlorohydrin rubber, epichlorohydrin-ethylene oxide rubber, epichlorohydrin-ethylene oxide-acrylic glycidyl ether terpolymer, urethane rubber, acrylic rubber, ethylene-propylene rubber, styrene rubber, butadiene rubber and natural rubber. They can be used singly or in admixture of two or more kinds.

As the mold release agent, there can be mentioned, for example, fatty acid or metal salt thereof (metallic soap) such as stearic acid or zinc salt of stearic acid; montanic acid; fatty ester; fatty chloride; amine-type fatty acid; amide-type fatty acid; wax such as carnauba wax and polymer-type wax and the like. They can be used singly or in admixture of two or more kinds.

The conductive skin part may contain, as necessary, additives such as plasticizer, stabilizer, antioxidant, antihydrolysis agent and the like.

In the material constituting the conductive skin part 3, the proportions of the carbon powder and the resin can be, for example, 100 parts by weight (the carbon powder) and 3 to 35 parts by weight (the resin). When the proportion of the resin is smaller than 3 parts by weight, the conductive skin part 3 is unable to have sufficient strength, and may be collapsed, for example, by the water formed during power generation of fuel cell. When the proportion of the resin is larger than 35 parts by weight, the conductivity required for the conductive skin part 3 cannot be secured.

The proportions of the carbon powder and the mold release agent can be, for example, 100 parts by weight (the carbon powder) and 0.1 to 3 parts by weight, preferably 0.5 to 2 parts by weight (the mold release agent). When the proportion of the mold release agent is smaller than 3 parts by weight, the conductivity required for the conductive skin part 3 can be secured.

In the present invention, the mold release agent is selectively added to the conductive skin part 3, and the conductive skin part 3 is bonded to the conductive core part

1 via conductive adhesive layer 2, and accordingly, there is
no possibility that the conductive skin part 3 is peeled from
the conductive core part 1.

The fuel cell separator of the present invention
5 can be produced by at least three kinds of methods depending
upon how the conductive skin part 3 is formed.

In the first production method, as shown in Fig.
2, a conductive skin part 3' is produced beforehand, and is
bonded with a conductive core part 1 using a conductive adhe-
10 sive. In the second production method, as shown in Fig. 3, a
laminate of a conductive core part and a conductive skin part
via a conductive adhesive is placed in a die and molded into
a separator shape. In the third production method, as shown
in Fig. 4, there are placed, in a die, a conductive core part
15 1 coated with a conductive adhesive and a material for the
conductive skin part to be formed on one or both sides of the
core part, and then molding is conducted.

In the present invention, as mentioned above, a
conductive core part 1 and a conductive skin part 3 are ad-
20 hered via a conductive adhesive layer 2, to obtain a fuel

cell separator. In this step as well, a known method can be used. There can be used, for example, die molding, injection molding, extrusion molding, roll molding or isostatic molding.

The present invention is described in more detail
5 below by way of Examples.

Examples 1 to 5

There were mixed, in a ball mill, 50 parts by weight of scaly graphite (average particle diameter = 3 μm), 50 parts by weight of acetylene black (average particle diameter = 40 nm) and 32 parts by weight of a phenolic resin, whereby a conductive adhesive was produced. As a core part, there was used a stainless steel sheet (flat sheet made of SUS 316, thickness = 0.1 mm, no groove). The above conductive adhesive was spray-coated on the whole surface of the
10 steel sheet and then dried to form a conductive adhesive layer having a thickness of 30 μm .
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As shown in Fig. 2, a raw material mixture for skin part shown in Table 1 (to this mixture, 1 part by weight of zinc salt of stearic acid per 100 parts weight of the conductive filler was added as a mold release agent) was fed in-
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to two same dies for separator molding, each consisting of a
ribbed half die and a non-ribbed half die, to mold two same
conductive skin parts. One of the half dies was removed from
each die (the ribbed half die was removed from one die, and
5 the non-ribbed half die was removed from the other die). Be-
tween the two remaining half dies (actually between the two
conductive skin parts) was placed the above-produced conduc-
tive core part covered with the conductive adhesive layer,
and pressing was made at 152°C at 120 kg/cm² for 5 minutes to
10 produce a separator of 2 mm in thickness having a conductive
core layer in the center.

This separator for fuel cell was measured for re-
sistivity and gas permeability. Further, the separator was
fitted to a repeated compression tester used in JIS K 6400 (a
15 test method for soft urethane foam), then subjected to 20
times repeated compression, and observed for the condition
after the test. Furthermore, the separator was integrated
into a solid polymer type fuel cell; clamping was made at a
pressure of 100 kg/cm²; in this state, the fuel cell was al-
20 lowed to generate electricity for 500 hours and there was

measured voltage reduction after 500 hours (initial voltage was taken as 100). After the electricity generation of 500 hours, the fuel cell was disassembled to observe the condition of the separator. The test results are shown in Table 1.

5 Examples 6 to 10

A fuel cell separator having a skin part made of a raw material mixture shown in Table 1 (to this mixture, 1 part by weight of zinc salt of stearic acid per 100 parts weight of the conductive filler was added as a mold release agent) was produced in the same manner as in Examples 1 to 5 except that there was used, as a material for core part, an aluminum sheet (a flat sheet of 0.1 mm in thickness having no groove), and evaluated in the same manners as in Examples 1 to 5. The results are shown in Table 1.

Table 1

	Example 1	Example 2	Example 3	Example 4	Example 5	Example 6	Example 7	Example 8	Example 9	Example 10
Core part	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Aluminum	Aluminum	Aluminum	Aluminum	Aluminum
Conductive filler	100	100	100	100	100	100	100	100	100	100
Resin	3	5	10	20	35	3	5	10	20	35
Resistivity (mΩ·cm)			9	18	34	4	5	8	16	32
Gas permeability (mL/m ² ·day·atm)	15	3	2	1	1	15	5	10	20	35
Condition of separator after 20 times repeated compression	A	A	A	A	A	A	A	A	A	A
Voltage after 500-hour power generation (initial voltage taken as 100)	94	97	97	97	94	94	97	97	97	94
Condition of separator after 500 hours	A	A	A	A	A	A	A	A	A	A

A: No problem. There is neither cracking nor peeling of skin part.

Conductive filler in skin part: natural graphite (average particle diameter; 30nm)

Examples 11 to 22

A fuel cell separator was produced in the same manner as in Example 4 except that there were changed the kind and composition of the conductive adhesive composing the
5 conductive adhesive layer and the thickness of the conductive adhesive layer, and evaluated in the same manners as in Examples 1 to 5. The results are shown in Table 2.

Table 2

	Example 11	Example 12	Example 13	Example 14	Example 15	Example 16	Example 17	Example 18	Example 19	Example 20	Example 21	Example 22
Conductive adhesive												
Natural graphite (av. Particle dia =20 μ m)	75	75	75	75	75	75	75	75	50	25	100	-
Acetylene black (av. Particle dia=40nm)	25	25	25	25	25	25	25	25	50	75	-	100
Penolic resin	67	67	67	67		150	32	10	67	67	67	67
Silicone rubber					67							
Thickness of conductive adhesive layer (μ m)	10	40	60	100	30	30	30	30	30	30	30	30
Core part	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel	Stainless steel
Skin part	100	100	100	100	100	100	100	100	100	100	100	100
Conductive filler	20	20	20	20	20	20	20	20	20	20	20	20
Resin	1	1	1	1	1	1	1	1	1	1	1	1
Separating agent	24	18	16	14	18	34	17	15	25	26	32	40
Resistivity (m Ω ·cm)	2	2	1	1	2	1	2	15	17	20	30	30
Gas permeability (ml/m ² ·day·atm)	A	A	A	A	A	A	A	A	A	A	A	A
Condition of separator after 20 times repeated compression	97	97	97	97	97	94	95	94	96	95	95	94
Voltage after 500-hour power generation (initial voltage taken as 100)	A	A	A	A	A	A	A	A	A	A	A	A
Condition of separator after 500 hours	A	A	A	A	A	A	A	A	A	A	A	A

A : No problem. There is neither cracking nor peeling of skin part.

Conductive filler in skin part: natural graphite (average particle diameter; 30nm)

Example 23

A fuel cell separator was produced in the same manner as in Example 4 except that as shown in Fig. 3, a conductive skin part molded in a flat sheet shape was laminated with a core part using a conductive adhesive to produce a separator precursor, the separator precursor was placed in a ribbed die for separator molding, and bonding between the conductive skin part and the core part was made. The fuel cell separator was evaluated in the same manner as in Examples 1 to 5. The results are shown in Table 3.

Example 24

As shown in Fig. 4, one half of a material for conductive skin part was placed in a lower ribbed die for separator molding, thereon was placed a core part coated with a conductive adhesive, thereon was placed other half of the material for conductive skin part, and molding was made. The fuel cell separator was evaluated in the same manners in Examples 1 to 5. The results are shown in Table 3.

Comparative Example 1

Molding was conducted using the same skin part

composition as in Example 2, to produce a fuel cell separator having a thickness of 1.0 mm. In the same manner as in Example 1, the separator was measured for resistivity and gas permeability, then subjected to 20 times repeated compression, and observed for the condition after the test. Furthermore, the separator was integrated into a solid polymer type fuel cell and clamping was made; the fuel cell was allowed to generate electricity for 500 hours and there was measured voltage reduction after 500 hours; after the electricity generation of 500 hours, the fuel cell was disassembled to observe the condition of the separator, in the same manner as in Example 1. The results are shown in Table 3.

Comparative Example 2

A liquid crystal polymer was injected onto the both sides of an aluminum sheet to produce a separator base material. Thereon was vapor-deposited gold to produce a fuel cell separator having a thickness of 1.0 mm. In the same manner as in Example 1, the separator was measured for resistivity and gas permeability, then subjected to 20 times repeated compression, and observed for the condition after the

test. Furthermore, the separator was integrated into a solid polymer type fuel cell and clamping was made; the fuel cell was allowed to generate electricity for 500 hours and there was measured voltage reduction after 500 hours; after the electricity generation of 500 hours, the fuel cell was disassembled to observe the condition of the separator, in the same manner as in Example 1. The results are shown in Table 3.

Comparative Example 3

Molding was conducted in the same manner as in Example 1 except that an aluminum mesh was used in the core part, to produce a fuel cell separator having a thickness of 1.0 mm. In the same manner as in Example 1, the separator was measured for resistivity and gas permeability, then subjected to 20 times repeated compression, and observed for the condition after the test. Furthermore, the separator was integrated into a solid polymer type fuel cell and clamping was made; the fuel cell was allowed to generate electricity for 500 hours and there was measured voltage reduction after 500 hours; after the electricity generation of 500 hours, the fu-

el cell was disassembled to observe the condition of the separator, in the same manner as in Example 1. The results are shown in Table 3.

Comparative Example 4

5 An aluminum sheet having a thickness of 1.0 mm was placed between two expanded graphite sheets and molding was made to produce a fuel cell separator having a thickness of 1.0 mm. In the same manner as in Example 1, the separator was measured for resistivity and gas permeability, then sub-
10 jected to 20 times repeated compression, and observed for the condition after the test. Furthermore, the separator was integrated into a solid polymer type fuel cell and clamping was made; the fuel cell was allowed to generate electricity for 500 hours and there was measured voltage reduction after 500
15 hours; after the electricity generation of 500 hours, the fuel cell was disassembled to observe the condition of the separator, in the same manner as in Example 1. The results are shown in Table 3.

Comparative Example 5

20 Molding was conducted in the same manner as in

Example 11 except that the thickness of the conductive adhesive layer was changed to 500 μ m, to produce a fuel cell separator. In the same manner as in Example 11, the separator was evaluated. The results are shown in Table 3.

5 Comparative Example 6

Molding was conducted in the same manner as in Example 4 except that the same composition of the conductive adhesive layer as the conductive skin part was employed (the mold release agent was included), to produce a fuel cell separator. In the same manner as in Example 4, the separator was evaluated. The results are shown in Table 3.

Table 3

	Example 23	Example 24	Comparative Example 1	Comparative Example 2	Comparative Example 3	Comparative Example 4	Comparative Example 5	Comparative Example 6
Conductive adhesive	Natural graphite (av. Particle dia=20 μ m) Acetylene black (av. Particle dia=40nm) Penolic resin						75	75
Thickness of conductive adhesive layer (μ m)							25	25
								1
							500	20
Core part	Stainless steel	Stainless steel		Aluminum sheet	Aluminum mesh		Stainless steel	Stainless steel
Resin				Liquid crystal polymer				
Vapor-deposited metal				Gold				
Skin part	100	100	100		100	Expanded graphite sheet	100	100
Conductive filler	20	20	5		20		20	20
Resin	1	1	1		1		1	1
Separating agent	18	25	408	400	300	300	450	400
Resistivity (m Ω ·cm)	2	4	30000	20000	15000	20000	4	20000
Gas permeability (ml/m ² ·day·atm)					B,C (interface between aluminum mesh and molded material)	B,C (interface between aluminum sheet and expanded graphite sheet)	A	C (interface between stainless steel and molded material)
Condition of separator after 20 times repeated compression	A	A	B	C (vapor-deposited portion)	Unable to measure.	Unable to measure.	30	Unable to measure.
Voltage after 500-hour power generation (initial voltage taken as 100)	97	94	Unable to measure.	Unable to measure.	Unable to measure.	Unable to measure.		
Condition of separator after 500 hours	A	A	B	B	B	B	A	C

A: No problem. There is neither cracking nor peeling of skin part.

B: Cracking appeared. Unusable as a fuel cell separator.

C: Peeling appeared. Unusable as a fuel cell separator.

Conductive filler in skin part: natural graphite (average particle diameter; 30nm)

In the fuel cell separator of the present invention, since the conductive core part and the conductive skin part including a mold release agent are adhered via the conductive adhesive layer, peeling hardly occurs between the
5 conductive core part and the conductive skin part, and there occurs no reduction in strength or gas non-permeability even when the separator is made in a thin sheet.

Since the conductive core part and the conductive skin part are tightly adhered via the conductive adhesive
10 layer, the present separator shows substantially no increase in resistance caused by increase in contact resistance.